

What is claimed is:

1. A process for variably preparing mixtures of optionally alkyl-substituted BDO, GBL and THF by two-stage hydrogenation in the gas phase of C<sub>4</sub> dicarboxylic acids and/or derivatives thereof, which comprises
  - a) in a first step in the gas phase, hydrogenating a gas stream of C<sub>4</sub> dicarboxylic acids and/or derivatives thereof over a catalyst at a pressure of from 2 to 100 bar and a temperature of from 200°C to 300°C in a first reactor in the presence of a catalyst in the form of shaped catalyst bodies having a volume of less than 20 mm<sup>3</sup>, said catalyst from 5 to 95% by weight of oxide of copper and from 5 to 95% by weight of an oxide having acidic sites, to give a stream mainly containing of optionally alkyl-substituted GBL and THF,
  - b) removing any succinic anhydride formed by partial condensation,
  - c) converting the products remaining predominantly in the gas phase in the partial condensation, THF, water and GBL, under the same pressure or under a pressure reduced by the pressure drops in the hydrogenation circuit and at a temperature of from 150 to 240°C, in a second reactor over a catalyst which ≤ 95% by weight of CuO and from 5 to 95% by weight of one or more oxides selected from the group of ZnO, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub>, CeO<sub>2</sub>, MgO, CaO, SrO, BaO, La<sub>2</sub>O<sub>3</sub> and Mn<sub>2</sub>O<sub>3</sub> to give a stream comprising a mixture of BDO, GBL and THF,
  - d) removing the hydrogen from the products and recycling it into the hydrogenation,
  - e) distillatively separating the products, THF, BDO, GBL and water, if appropriate recycling a GBL-rich stream into the second reactor or if appropriate discharging it, and working up BDO, THF and GBL distillatively,and setting the ratio of the products, THF, GBL and BDO, relative to one another within the range from 10 to 100% by weight of THF, from 0 to 90% by weight of GBL and from 0 to 90% by weight of BDO only by varying the temperatures in the two hydrogenation zones and also if appropriate the GBL recycle stream.
2. The process according to claim 1, wherein the partial condensation of the SA is designed as a circulation quench cycle.

3. The process according to claims 1 or 2, wherein the evaporation of the recycled GBL or GBL/water mixture is effected in a countercurrent apparatus, preferably a stripping column, with the GBL/THF-laden cycle gas hydrogen.
- 5 4. The process according to claims 1 to 3, wherein the partial condensation of the succinic anhydride and the evaporation of the GBL or GBL/water recycle stream are combined in one apparatus, preferably in a countercurrent stripping column with external quench circuit, and the succinic anhydride is discharged as the bottom effluent together with residual GBL, water and high-boiling secondary components.  
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5. The process according to any of claims 1 to 4, which is carried out continuously.
- 15 6. The process according to any one of claims 1 to 5, wherein the inlet temperature in the first reactor is at values of from 200°C to 300°C, preferably from 235 to 270°C, and from approx. 5 to 15°C, preferably from approx. 10 to 15°C, below the hotspot temperature.
- 20 7. The process according to any of claims 1 to 6, wherein the temperature increase in the second reactor is not more than 90°C, preferably not more than 40°C, in particular not more than 20°C.
- 25 8. The process according to any of claims 1 to 7, wherein the inlet temperature in the second reactor is at values between 150°C and 270°C, preferably between 175°C and 195°C.
- 30 9. The process according to any of claims 1 to 8, wherein both hydrogenation stages are carried out at pressures of from 2 to 100 bar, preferably from 2 to 60 bar, in particular from 15 to 35 bar.
- 35 10. The process according to any of claims 1 to 9, wherein the catalyst hourly space velocity of the first hydrogenation stage is in the range from 0.02 to 2 kg of reactant/l of catalyst hour, in particular from 0.05 to 1 kg of reactant/l of catalyst • hour.
- 40 11. The process according to any of claims 1 to 10, wherein the catalyst hourly space velocity of the second hydrogenation stage is in the range from 0.02 to 2 kg of reactant/l of catalyst • hour, in particular from 0.1 to 1 kg of reactant/l of catalyst hour.
12. The process according to any of claims 1 to 11, wherein the molar hydrogen/reactant ratio in the first hydrogenation stage is at values of from 20 to 650,

preferably from 20 to 200, in particular from 40 to 150, most preferably from 50 to 100.

- 5 13. The process according to any of claims 1 to 12, wherein the molar hydrogen/GBL ratio in the second hydrogenation stage is at values of from 20 to 1000, preferably from 50 to 400, in particular from 100 to 300.
- 10 14. The process according to any of claims 1 to 13, wherein the reactor used in the first hydrogenation stage is a fixed bed reactor, preferably a tubular reactor, a shaft reactor, a fluidized bed reactor or a reactor having internal heat removal, in particular a shaft reactor.
- 15 15. The process according to any of claims 1 to 14, wherein the reactor used in the second hydrogenation stage is a fixed bed reactor, preferably a tubular reactor, a tube bundle reactor, a fluidized bed reactor or a reactor having internal heat removal, in particular a shaft reactor.
- 20 16. The process according to any of claims 1 to 15, wherein the volume of the individual shaped body in the first hydrogenation stage is  $< 10 \text{ mm}^3$ , preferably  $< 6 \text{ mm}^3$ .
- 25 17. The process according to any of claims 1 to 16, wherein the CuO  $< 80\%$  by weight, preferably  $< 70\%$  by weight, in particular from 10 to 65% by weight, of CuO, and  $> 20\%$  by weight, preferably  $> 30\%$  by weight, in particular from 35 to 90% by weight, of an oxide having acidic sites are present.
- 30 18. The process according to any of claims 1 to 17, wherein the oxide having acidic sites is  $\text{Al}_2\text{O}_3$ .
- 35 19. The process according to any of claims 1 to 18, wherein the catalyst of the first hydrogenation stage one or more further metals or a compound thereof, preferably an oxide from the group consisting of the elements of groups 1 to 14 of the Periodic Table of the Elements are present in the catalyst, preferably a substance from the group consisting of  $\text{ZrO}_2$ ,  $\text{TiO}_2$ ,  $\text{CaO}$ ,  $\text{Na}_2\text{O}$ ,  $\text{Mn}_2\text{O}_3$ ,  $\text{BaO}$ ,  $\text{SiO}_2$  and  $\text{MgO}$ .
- 40 20. The process according to any of claims 1 to 19, wherein the shaped catalyst body is in the form of an extrudate.
21. The process according to any of claims 1 to 20, wherein the catalyst of the second hydrogenation stage, in addition to CuO, oxides selected from the group of  $\text{ZnO}/\text{Al}_2\text{O}_3$  mixtures, delta-, theta-, alpha- and eta-modifications of  $\text{Al}_2\text{O}_3$ , and mixtures which comprise  $\text{Al}_2\text{O}_3$  and at least one component from the group of

SiO<sub>2</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub> on the one hand and from the group of ZnO, MgO, CaO, SrO and BaO on the other, or which contain at least one component from the group of SiO<sub>2</sub>, TiO<sub>2</sub>, ZrO<sub>2</sub> on the one hand and from the group of ZnO, MgO, CaO, SrO and BaO on the other.

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22. The process according to any of claims 1 to 4, wherein the catalyst of the second hydrogenation stage comprises oxides selected from ZnO, ZnO/Al<sub>2</sub>O<sub>3</sub> mixtures in a weight ratio of from 100:1 to 1:2 and mixtures of SiO<sub>2</sub> with MgO, CaO and/or ZnO in a weight ratio of from 200:1 to 1:1.

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23. The catalyst according to any of claims 1 to 20, which is activated by reduction, preferably by treatment with hydrogen or a hydrogen/inert gas mixture, before or after installation into the reactor and before use in the hydrogenation reaction.